

# Optimizing Floating Wind Turbine Design

## The Role of Tower Eigenfrequency in Dynamic Loads

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A planet powered by  
floating offshore wind





# Principle Power: proven technology and experience for a planet powered by floating offshore wind



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Globally patented and proven floating platform technology with 75MW in operation and 30MW under construction (over 800 GWh energy produced)



>7 GW global project pipeline secured & serving clients in all key floating offshore wind markets (14+ GW under design contract)



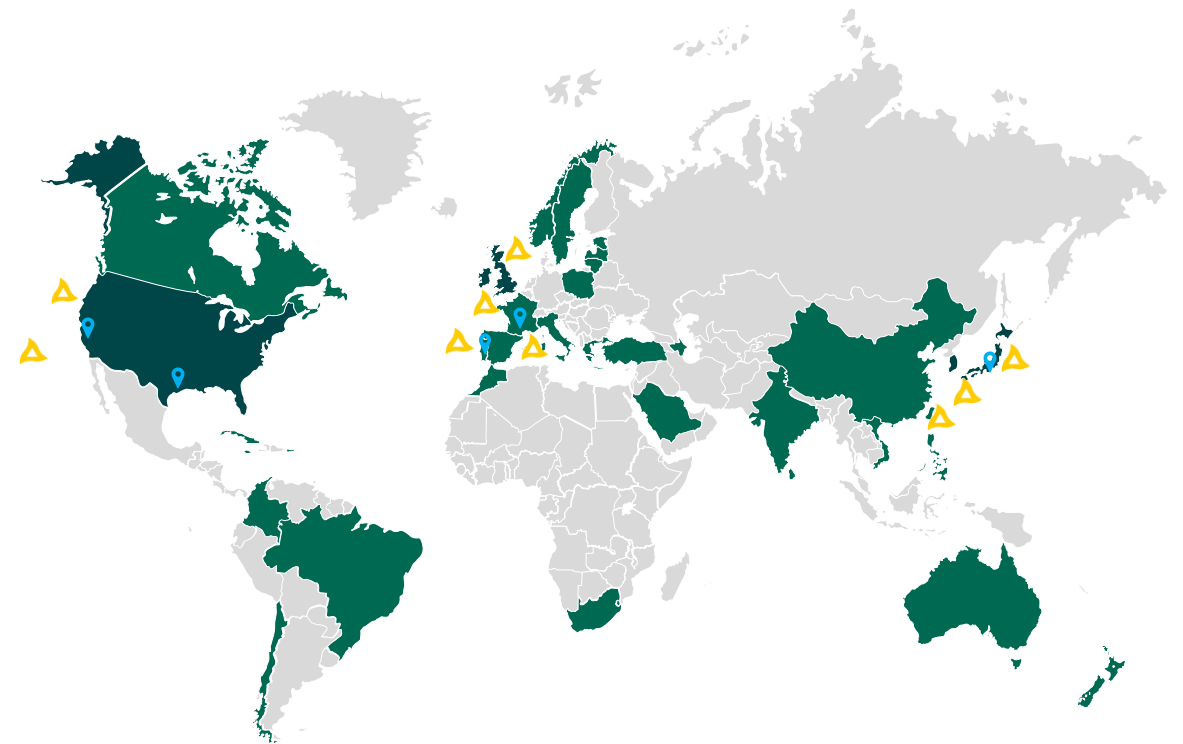
Proven floating wind services for successful and bankable projects spanning full lifecycle: engineering, execution, and O&M



Experts in WTG integrated load analysis, with mature, validated processes delivering optimal system performance & minimum risk



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● Existing developments and/or strong market potential

● Promising market

📍 Office location

▲ Project pipeline



# ReaLCoE – Objective: To reduce WECs electricity prices

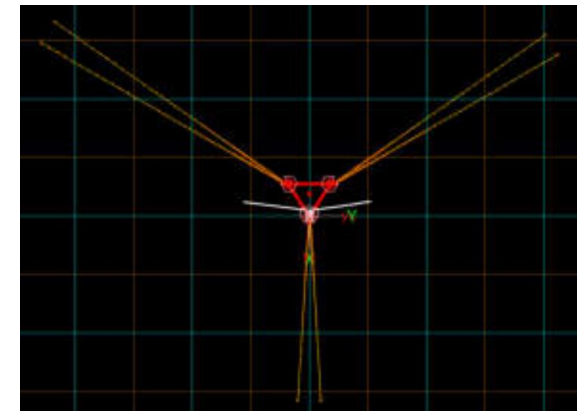
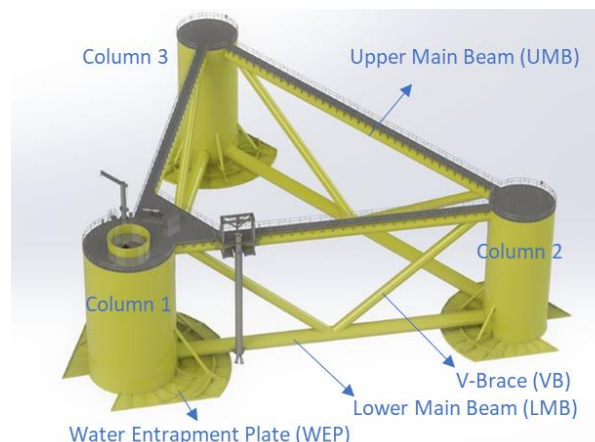


ReaLCoE is an **EU-funded project** to develop more efficient offshore wind energy converters (WECs). These WECs will produce clean energy at a lower cost than conventional and other renewable sources. By increasing the capacity of WECs to 14-16 MW, ReaLCoE aims to **achieve electricity prices as low as 35-50 €/MWh**. This would reduce energy costs and boost the European energy sector, leading to sustainable growth and job creation.



## WP1.3 - Floating conceptual design key objectives were:

- Define the design basis for the floating concept study (WindFloat-T concept).
- Design a preliminary WindFloat platform with a 15+MW turbine, with a catenary mooring system.
- Benchmark simulation tools (HAWC2 and Orcaflex) to assess loads on the turbine and platform.





# ReaLCoE – Overview WP1.3 – Main Configuration and Process

Wind turbine and tower modelling

- Fixed condition model.
- Eigenfrequency calculation.
- Wind turbine benchmark with HAWC2.

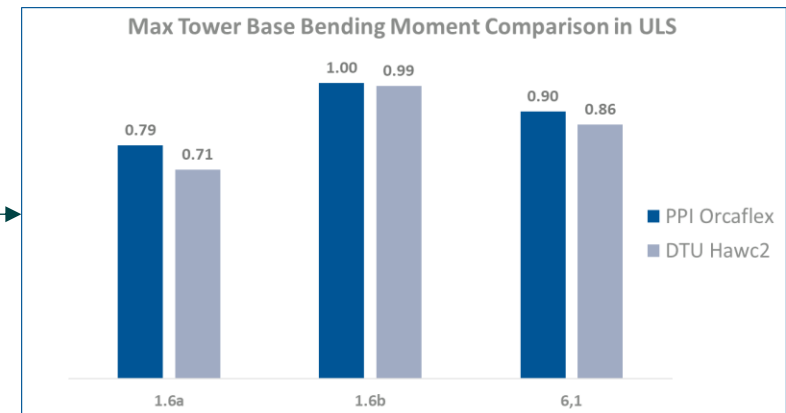
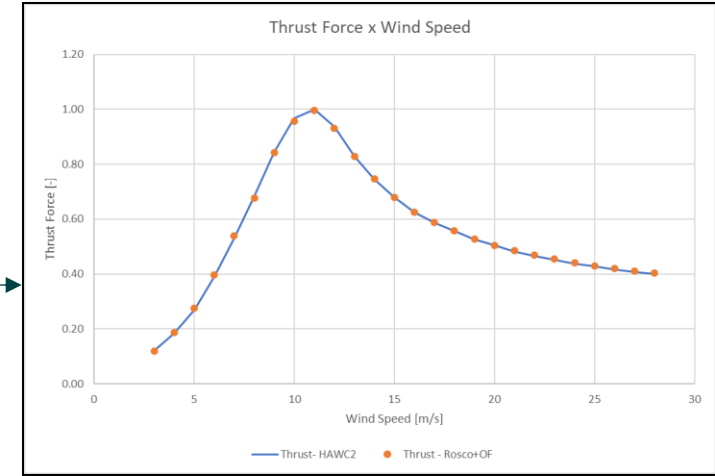
Floating model

- Floater sizing.
- Eigenfrequency calculation.
- ULS/FLS analysis.
- Mooring system development.

Post-processing

- Compare results with HAWC2.
- Controller analysis and improvements.
- Analysis in mooring configuration.

DLC	Turbine Status
1.2	Production
1.6	Production
5.1	Emergency shutdown
6.1	Parked

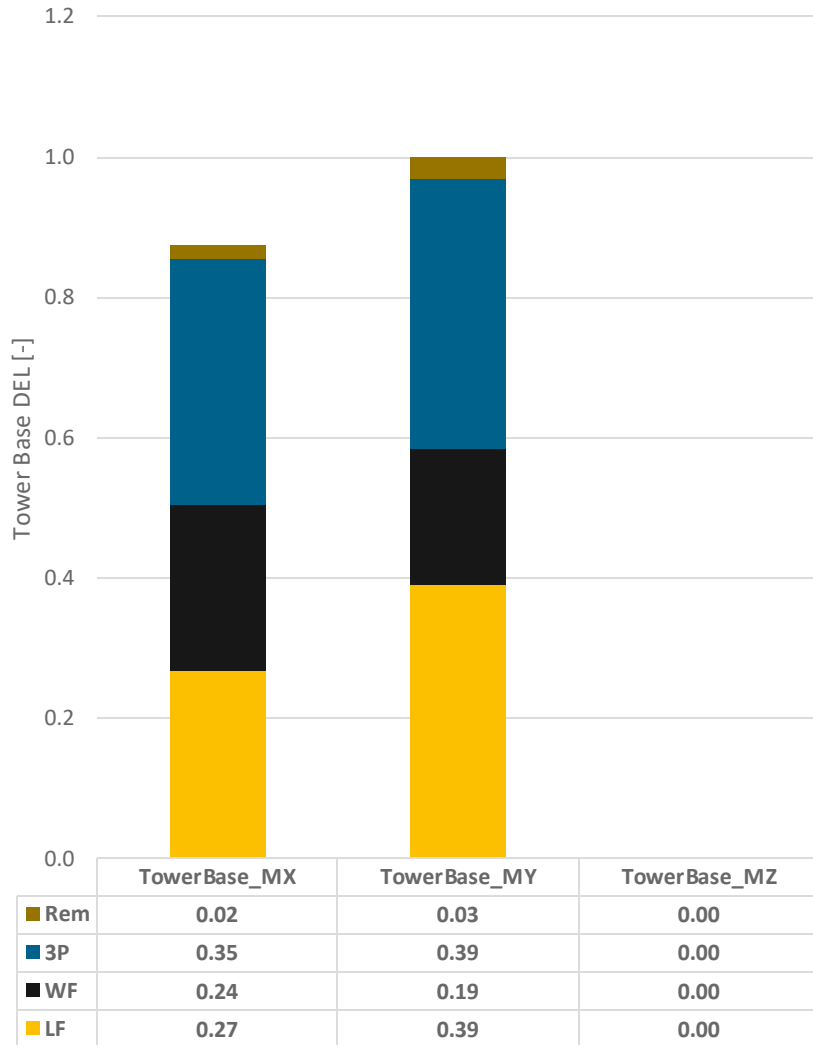




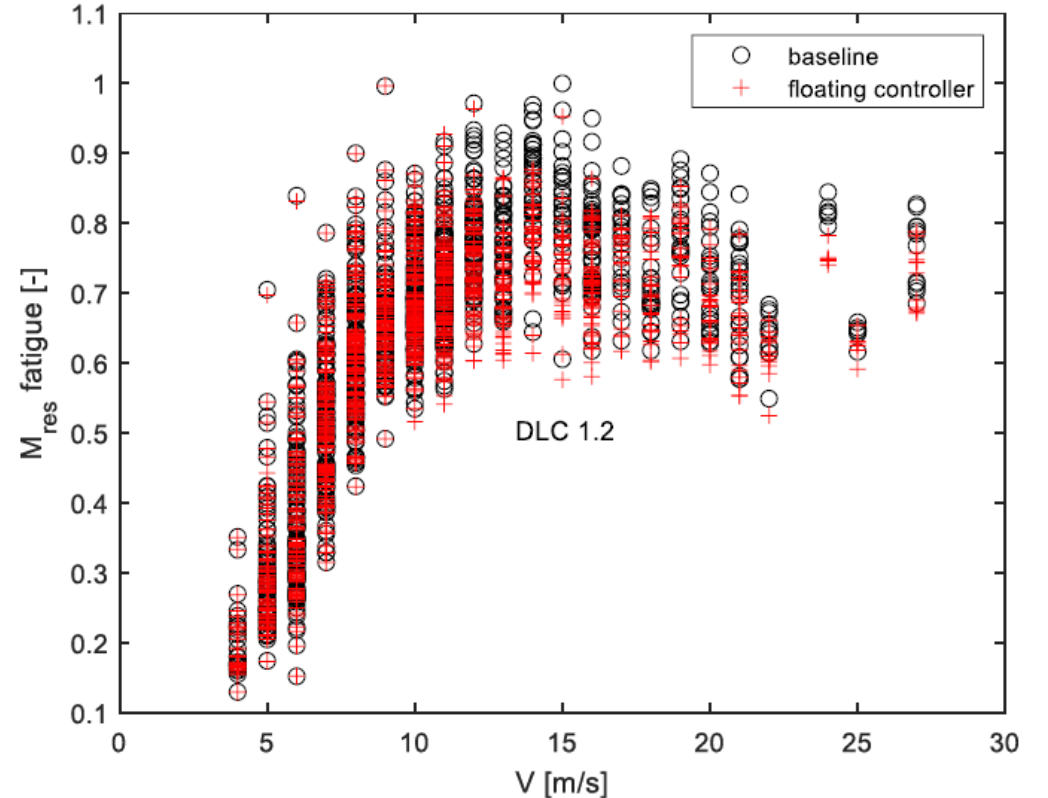
# 3P Impact in The Tower Damage Equivalent Load - ReaLCoE



### Tower Damage Equivalent Load



- Damage Equivalent Load coming from wind turbine is significant.
- DTU and PPI have tuned the controller for floating conditions, but schedule was relatively short to develop new controllers.
- It would be beneficial to explore further tuning options to potentially reduce FLS and ULS loads.



- LF: Low Frequency
- WF: Wave Frequency
- 3P: Blade Passing Frequency
- Rem: Remainder Frequency



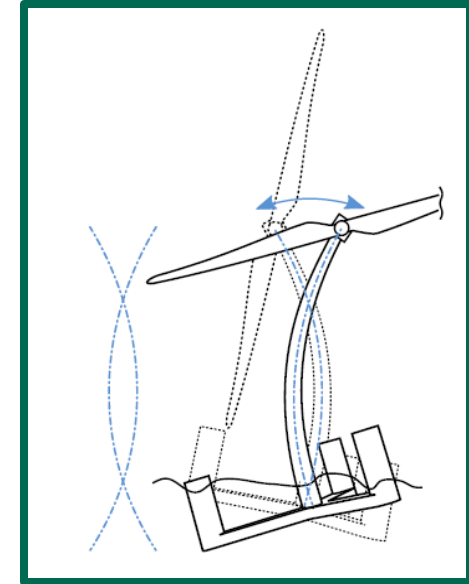
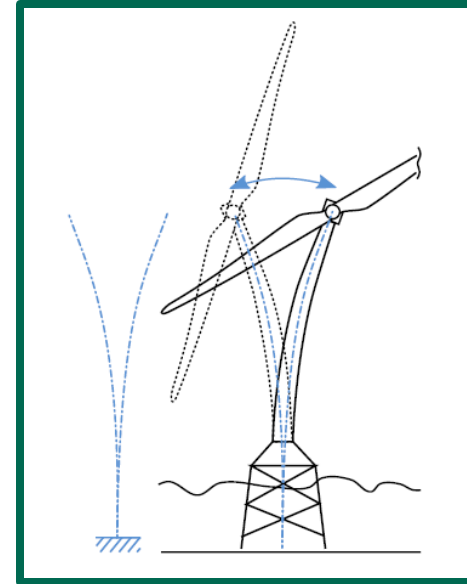


# Tower Eigenfrequency increases in Floater Configuration

Tower EF is affected by:

- Its foundation:
  - The tower system of a floating turbine **behaves like an unfixed beam** that can oscillate freely in all directions.
  - **The natural frequency of the tower increases** when comparing a floating turbine with a fixed turbine.
  - The equation shows the effect of the change in the first tower mode, assuming a constant homogeneous beam.\*
- Varying the tower **diameter and thickness**.
- The **mass/inertia of the RNA**.
- Need to consider the **mass/inertia of the floater** and, the stiffness of the system.
- The **flexibility of the floater**.
- E.g.in ReaLCOE:

ReaLCOE	
Mode	EF Difference between fixed and float condition [%]
Side-Side	22.2%
Fore-Aft	31.5%



$$\omega_0 = (\lambda l)^2 \sqrt{\frac{EI}{\rho A l^4}}$$

Eigenvalue

Bending Stiffness

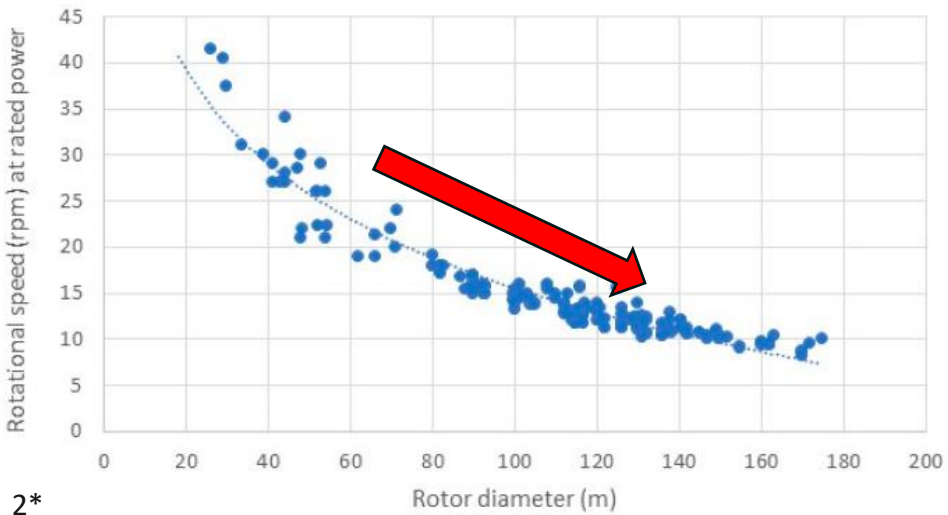
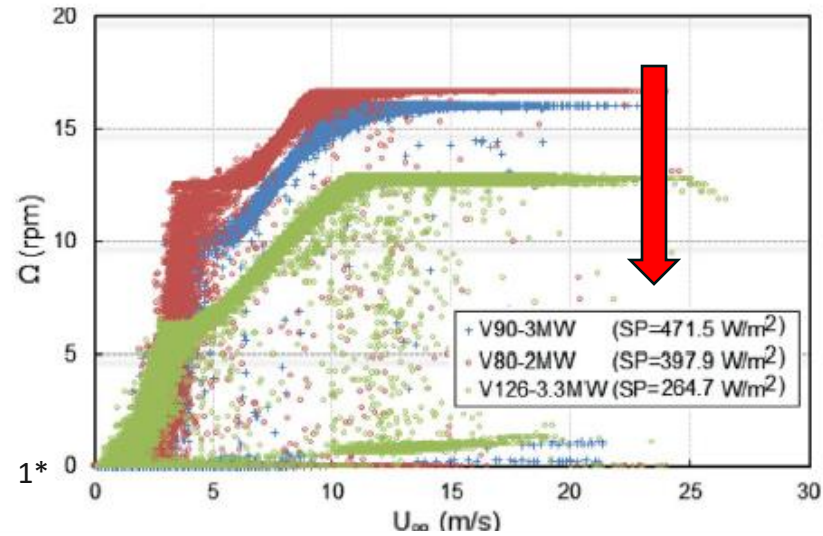
Length

Density

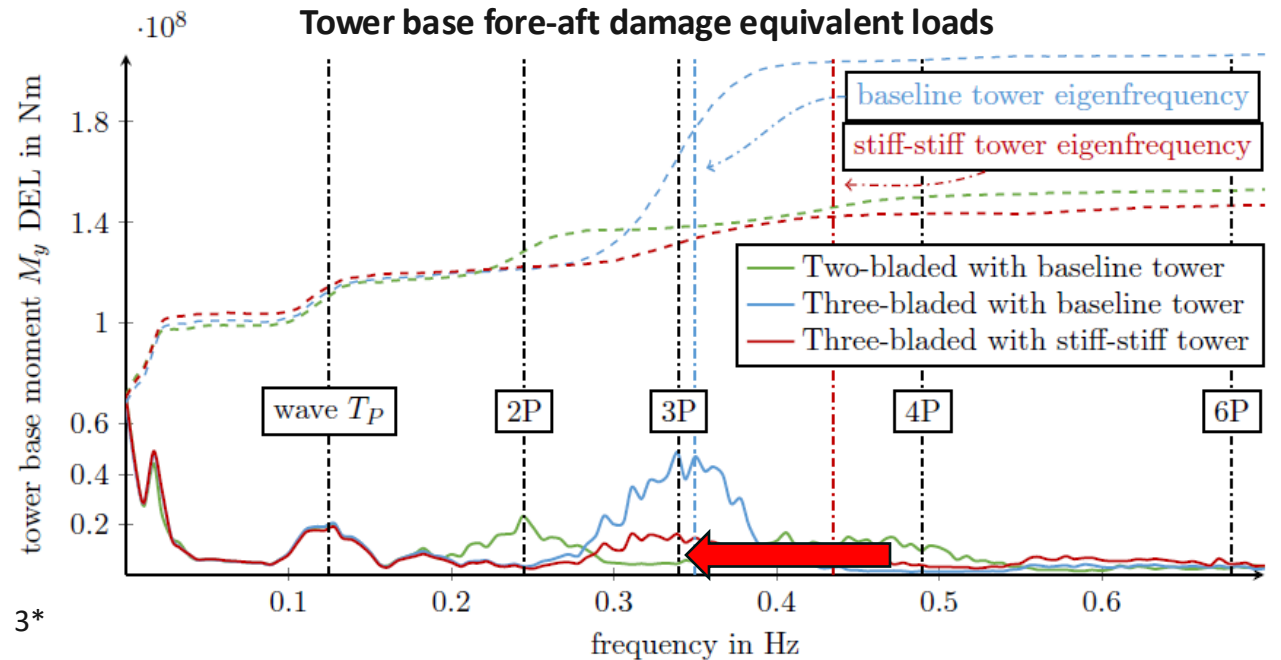
Cross-section Area



# Larger wind turbines have rotated at lower speed



- Historically, larger wind turbines have **rotated at lower speeds**.
- As a result, the WTM 15+MW **reduces the soft-stiff zone window** in floater conditions. However, this increases the margin of the stiff-stiff towers solutions.
- The stiff-stiff solution needs to be addressed with lightweight platforms designed for stiff conditions.



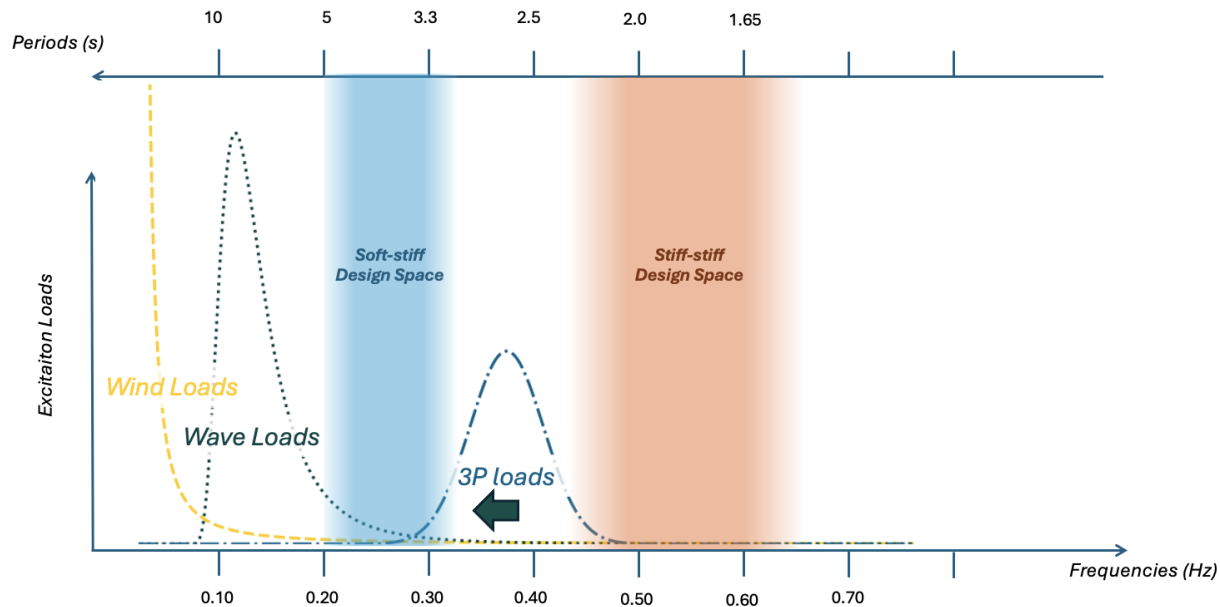


# Design space for 15+ MW wind turbines

300  
x  
30

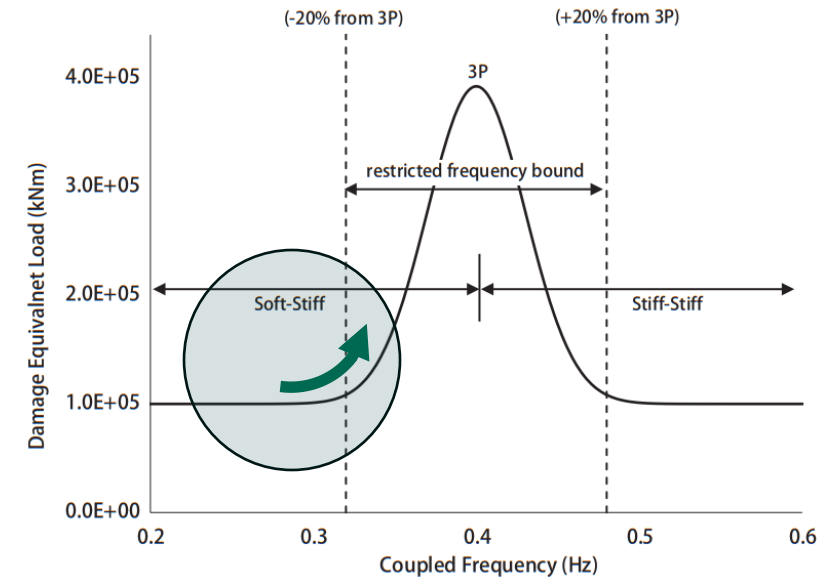
## Design Space for Floating Wind Turbines

- So-called “soft-stiff” or “stiff-stiff” design space.
- Defined by where the coupled system eigenfrequency (EF) lies.
- For any WTG / platform design, keeping a safety margin between these frequencies is crucial to avoid a resonant response of the system, which could lead to severe fatigue damage.
- As the WTG size increases, the soft-stiff design space decreases as 3P loads frequency decreases (WTG spinning slower)



## Wind Turbine Manufacturer’s Challenge

- The WTG **soft-stiff** approach exposed to risk of a vicious cycle of increasing stiffness and thereby increasing fatigue loads
  - Manageable with right tools and contingencies upfront
- Soft-stiff diverging design spiral:
  - If system shows high fatigue loads (EF too close to 3P)
  - Then, add reinforcements, increasing stiffness and increasing EF
  - Then, higher fatigue loads requires adding more reinforcements





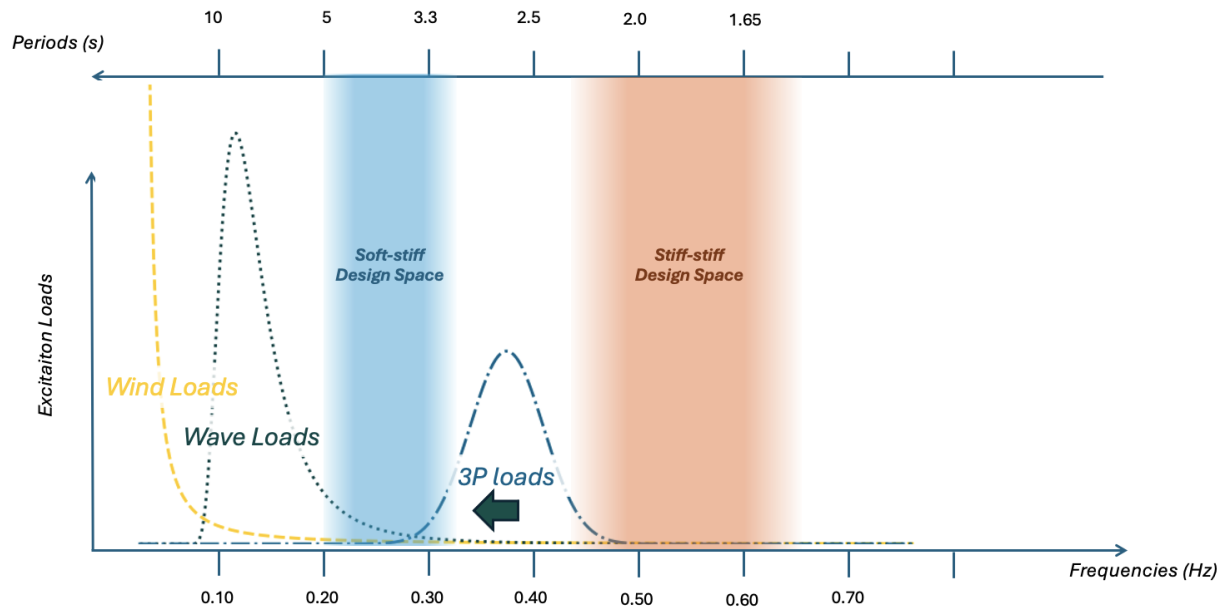


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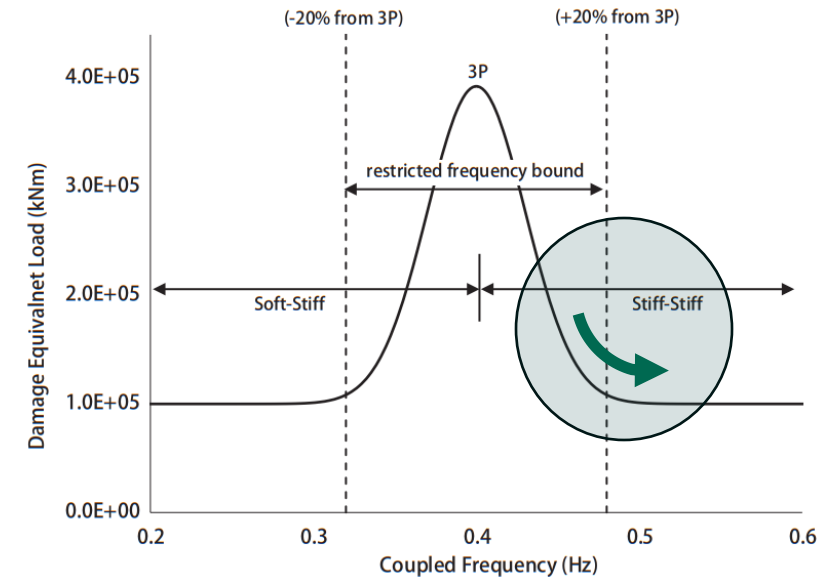
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## The WTG stiff-stiff approach

- The coupled system EF needs to be significantly increased
- Drivers are stiffness and mass/inertia





# WindFloat® central platforms are preferred for stiff-stiff towers

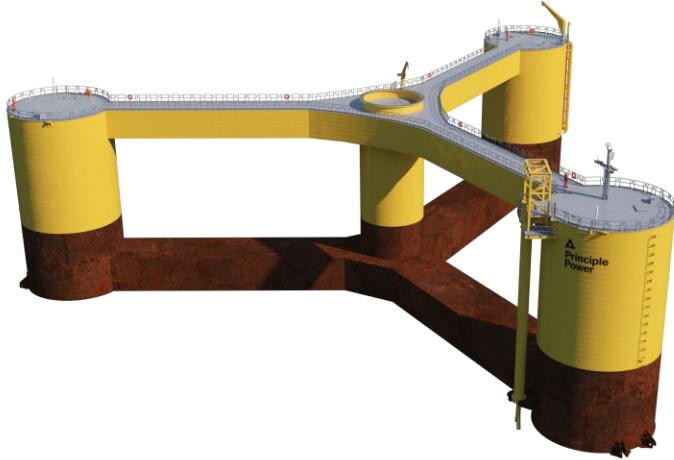


Illustration of WindFloat TC



Illustration of WindFloat FC



**Bankable from the beginning: natural evolution from WindFloat® product line**

- Central turbine designs leverage four generations of WindFloat® heritage
- Platforms rearranges bankable modules:
  - WTG supported by continuous diameter shaft that reaches keel level for structural continuity (from WindFloat T);
  - Columns from WindFloat T & F
  - pontoons and UMB (from WindFloat F)



**Central-column, pontoon-based design for weight-efficient & flexible design**

- Compact configuration minimizes column size & footprint
- Pontoon enables integration in shallow water ports (>8m);
- Symmetry reduces destabilizing yaw moment and direction-independent EF.
- Flexibility to manage any late weight deviations in as-designed or as-built system



**Columns and major components enable access to tubular or flat panel supply chains**

- Identical geometries and fabrication methods to WindFloat T (e.g., Tubular columns) and WindFloat F (e.g., hexagonal columns)
- Compatible with existing automated tubular and flat-panel fabrication lines
- Welded connections for long reliable lifetimes in harsh offshore environments



**Optimized for Industrialized delivery**

- Modular “block” subcomponent philosophy for columns, pontoons, and box braces
- Blocks manufactured indoor in serial lines for high throughput and quality
- Simple geometries for high density transportation and wet/dry storage



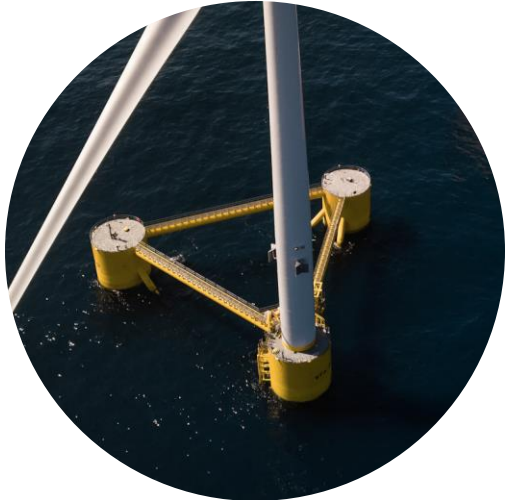
**Hull Trim System**

- Fully redundant, closed loop system to transfer water ballast between columns
- Maximizes AEP and reduce WTG structural loads versus passive systems



# Windfloat® design portfolio enables wind turbine standardization and maximizes compatibility with existing fabrication capabilities

WTGs with “Soft-Stiff” Tower



**WindFloat T**  
Tubular Design, with unparallel operational track record



**WindFloat F**  
Flat-panel, pontoon-based solution, with established flat panel construction methods

WTGs with “Stiff-Stiff” Towers



**WindFloat TC**  
Tubular, with center column, optimized for 15+ MW “Stiffer” Towers

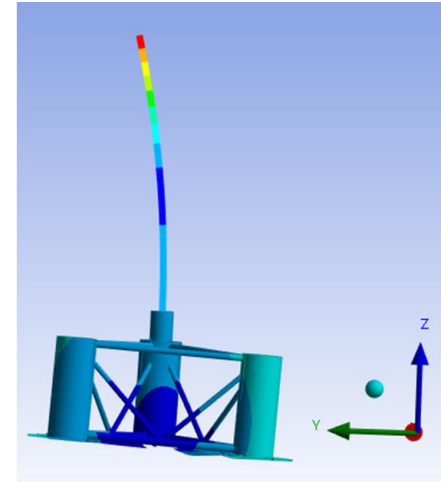


**WindFloat FC**  
Flat Panel, center column, optimized for 15+ MW “Stiffer” Towers

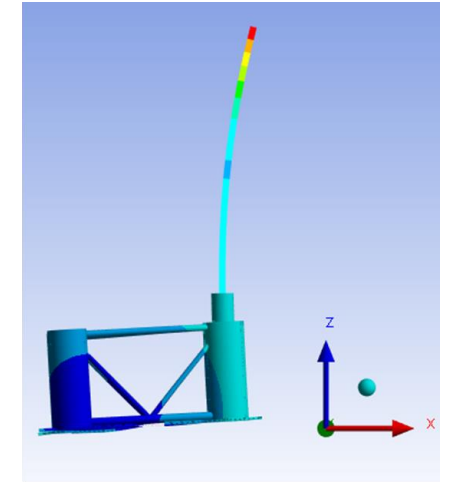


# Eigenfrequency on project execution

- **Eigenfrequency** and **contingency management** are complex topics in floating wind projects due to the very “coupled” nature of the designed system.
- **Eigenfrequency calculation methodologies** are company-dependent (existing standards deal with integrity, not system performance).
  - Requires a deep technical engagement on both sides (WTG and Platform).
  - Must align on conventions, assumptions, model setups, etc.
- WTM and platform designer need to **run Integrated Load Analysis (ILA)** with inputs from other party.
  - Modeling and exchanging data are critical for efficient ILA convergence.
  - Our processes and models are proven (3 complete project cycles).
- System eigenfrequency is a **shared interface between developer, WTM and designer** that cannot be transferred and must be actively managed:
  - Shared responsibility define “coupled-system” inputs performed with imperfect information about the full system behavior (e.g., no blade model).
  - Design Basis should define process from engineering to commissioning, including measurement of as built performance during operations.
- Principle Power is applying our lessons learned **to build robust processes for commercial scale projects.**



Mode 7 - SS



Mode 8 - FA





## Please reach out for additional information

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